BAKER (MICHAEL) JR INC BEAVER PA F/G 13/13
NATIONAL DAM INSPECTION PROGRAM, PURDY (STUMP POND) DAM. (NDI N--ETC(U)
FEB 81 J A DZIUBEK DACW31-81-C-0011 AD-A099 092 UNCLASSIFIED NL 1 ... / Alle Alle Seguida END DATE 6⊶8I DTIC

RIVER BASIN

SALT LICK CREEK, SUSQUEHANNA COUNTY **PENNSYLVANIA**

PURDY (STUMP POND) DAM

NDI No. PA 00063 **PennDER NO. 58-11**

Dam Owner: Pennsylvania Fish Commission

PHASE I INSPECTION REPORT

NATIONAL DAM INSPECTION PROGRAM

DACW 31-81-C-0611

DEPARTMENT OF THE ARMY

Baltimore District, Corps of Engineers Baltimore, Maryland 21203

prepared by

MICHAEL BAKER, JR., INC.

Consulting Engineers 4301 Dutch Ridge Road Beaver, Pennsylvania 15009

February 1981

SUSQUEHANNA RIVER BASIN



PURDY (STUMP POND) DAM SUSQUEHANNA COUNTY, COMMONWEALTH OF PENNSYLVANIA NDI No. PA 00063 PennDER No. 58-11

PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM.

Port (1) Dayr. (1) Line THE THE Pennist River 1-1. Suozu tor a come de la come de la la Sugar la a C cuto Prosylvinia

Prepared for: DEPARTMENT OF THE ARMY

Baltimore District, Corps of Engineers
Baltimore, Maryland 21203

Prepared by:

MICHAEL BAKER, JR., INC. Consulting Engineers 4301 Dutch Ridge Road

Beaver, Pennsylvania 15009

//: Feb. 3.2.3981

PA MIN 1121-12 (- 1711)

DISTRIBUTION STATEMENT A

Approved for public release: Distribution Unlimited

4/11/11

PREFACE

This report is prepared under guidance contained in the "Recommended Guidelines for Safety Inspection of Dams," for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established guidelines, the spillway design flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The spillway design flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

í

PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM

Purdy (Stump Pond) Dam, Susquehanna County, Pennsylvania NDI No. PA 00063, PennDER No. 58-11 Salt Lick Creek Inspected 27 October 1980

ASSESSMENT OF GENERAL CONDITIONS

Purdy (Stump Pond) Dam is owned by the Pennsylvania Fish Commission and is classified as a "Significant" hazard - "Small" size dam. The dam was found to be in fair overall condition at the time of inspection.

Hydraulic/hydrologic evaluations, performed in accordance with procedures established by the Baltimore District, Corps of Engineers, for Phase I Inspection Reports, revealed that the spillway will not pass the 100-year flood without overtopping the dam. A spillway design flood (SDF) in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF) is required for Purdy Dam. Because the dam is on the low end of the "Small" size category in terms of height and storage capacity, the 100-year flood was chosen as the SDF. During the 100-year flood, the dam is overtopped by a maximum depth of 4.32 feet for a total duration of 40.83 hours. spillway is therefore considered "Inadequate." It is recommended that the owner immediately initiate an engineering study to further evaluate the spillway capacity and develop recommendations for remedial measures to reduce the overtopping potential of the dam.

Several items of remedial work should be immediately initiated by the owner. Item I below should be completed by a qualified professional engineer experienced in the design of hydraulic structures for dams. These include:

- 1) Initiate an engineering study to further evaluate the spillway capacity and develop recommendations for remedial measures to reduce the overtopping potential of the dam.
- 2) Fill the erosion gully at the right downstream abutment of the dam and reseed the area.
- 3) Remove the debris and silt at the entrance to the spillway.
- 4) Provide means to draw down reservoir during an emergency.

PURDY (STUMP POND) DAM

In addition, the following operational measures are recommended to be undertaken by the owner:

- 1) Develop a detailed emergency operation and warning system.
- 2) During periods of unusually heavy rain, provide around-the-clock surveillance of the dam.
- 3) When warning of a storm of major proportions is given by the National Weather Service, activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operation procedures and records be developed and implemented. A plan for emergency drawdown of the reservoir should be developed in case an emergency drawdown should become necessary. These should be included in a formal maintenance and operations manual for the dam.

Submitted by:

MICHAEL BAKER, JR., INC.

John A. Dziubek, P.E.

Engineering Manager-Geotechnical

19 February 1981 Date:

Approved by:

DEPARTMENT OF THE ARMY

BALTIMORE DISTRICT, CORPS OF ENGINEERS

JAMES W. PECK

COL, Corps of Engineers

District Engineer

Date: /3 MAR ()

PURDY (STUMP POND) DAM

TABLE OF CONTENTS

			Page
Section	1	- Project Information	1
Section	2	- Engineering Data	4
Section	3	- Visual Inspection	6
Section	4	- Operational Procedures	7
Section	5	- Hydraulic/Hydrologic	8
Section	6	- Structural Stability	10
Section	7	- Assessment, Recommendations/Remedial	11

APPENDICES

- Appendix A Visual Inspection Check List, Field Sketch, Top of Dam Profile, and Typical Cross-Section
- Appendix B Engineering Data Check List
- Appendix C Photograph Location Plan and Photographs Appendix D - Hydrologic and Hydraulic Computations
- Appendix E Plates Appendix F Regional Geology

PHASE I REPORT NATIONAL DAM INSPECTION PROGRAM PURDY DAM NDI No. PA 00063, PennDER No. 58-11

SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

- a. Authority The Dam Inspection Act, Public Law 92-367, authorized the Secretary of the Army, through the Corps of Engineers, to initiate a program of inspection of dams throughout the United States.
- b. Purpose of Inspection The purpose of the inspection is to determine if the dam constitutes a hazard to human life or property.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances - Purdy Dam is a stone masonry dam. Earthfill was placed between the outside walls and a masonry cap on top. The height of the dam is 7.4 feet and the length is 52 feet. The width at the crest is 3.5 feet with the downstream slope being in a series of terraces and vertical walls. The upstream slope appears to be similar to the downstream slope but is covered with a great deal of debris and silt and could not be observed.

The spillway is located immediately to the right of the center of the dam and consists of a stone broad crested weir and chute. The spillway crest is 11 feet long perpendicular to the direction of flow. The flow from the spillway cascades over several terraces in the spillway and over a vertical drop at the downstream end. The plunge pool is stone-lined.

There are no outlet works for the dam.

b. Location - Purdy Dam'is located on Salt Lick Creek approximately 3.2 miles east-southeast of New Milford in New Milford Township, Susquehanna County, Pennsylvania. The coordinates of the dam are N 41° 51.7' and W 75° 40'. The dam can be found on the Harford, PA USGS 7.5 minute topographic quadrangle.

- c. Size Classification The height of the dam is 7.4 feet and the reservoir volume is 62 acre-feet at the minimum top of dam [Elevation 1409.6 feet Mean Sea Level (ft. M.S.L.)]. The dam is therefore in the "Small" size category.
- d. Hazard Classification If the dam were to fail, property damage may occur to one trailer and two homes 10,000 feet downstream from the dam but loss of life is unlikely. There may also be damage to PA Route 492 which passes over the downstream channel 9000 feet downstream from the dam. The dam is therefore classified in the "Significant" hazard category.
- e. <u>Ownership</u> The dam and reservoir are owned by the Pennsylvania Fish Commission. The person responsible for maintenance and operations of the dam is Mr. Charles Rupert, Area III Maintenance Manager, Box 88, Sweet Valley, Pennsylvania 18656.
- f. Purpose of Dam The dam was originally constructed for water power, but is now used for fishing.
- g. <u>Design and Construction History</u> There is no information available on the construction date or company responsible for designing and constructing the dam. The earliest records of the dam in PennDER File No. 58-11 date back to 1920.
- h. Normal Operating Procedures The reservoir is maintained at the crest of the spillway (Elevation 1409.0 ft. M.S.L.). The dam is visited once a month during the late fall and winter, and approximately every other week or more frequently during the spring, summer, and early fall.

1.3 PERTINENT DATA

a.	Drainage Area (square miles) -	5.63
b.	Discharge at Dam Site (c.f.s.) -	
	Maximum Known Flood (1977) - Spillway Capacity at Maximum Pool	115
	(El. 1409.6 ft. M.S.L.) -	20

c. Elevation (feet above M.S.L.)* -

Design Top of Dam -	Unknown
Minimum Top of Dam -	1409.6
Maximum Design Pool -	Unknown

^{*}All elevations are referenced to the spillway crest, El. 1409.0 ft. M.S.L. as estimated from the USGS 7.5 minute topographis quadrangle, Harford, Pennsylvania.

	Spillway Crest - Streambed at Toe of Dam - Maximum Tailwater of Record -	1409.0 1402.2 Unknown
d.	Reservoir (feet) -	
	Length of Maximum Pool (El. 1409.6 ft. M.S.L.) - Length of Normal Pool (El. 1409.0 ft. M.S.L.) -	1825 1800
е.	Storage (acre-feet) -	
	Top of Dam (El. 1409.6 ft. M.S.L.) - Normal Pool (El. 1409.0 ft. M.S.L.) -	62 54
f.	Reservoir Surface (acres) -	
	Top of Dam (El. 1409.6 ft. M.S.L.) - Normal Pool (El. 1409.0 ft. M.S.L.) -	12.70 11.94
g.	Dam -	
	Type - Stone wall dam with earthfill and mas Total Length (feet) - Height (feet) - Design - Field - Top Width (feet) - Side Slopes - Upstream - Downstream - Zoning - Impervious Core - Cut-off - Drains -	onry cap 52 Unknown 7.4 3.5 Vertical Vertical None None Unknown None
h.	Diversion and Regulating Tunnels -	None
i.	Spillway -	
	Type - Stone broad crested weir Location - Right of center of dam Length of Crest Perpendicular to Flow (feet) - Crest Elevation (ft. M.S.L.) - Gates - Downstream Channel - Stone-lined plunge pool and downstream channel	11 1409.0 None
j.	Outlet Works -	None

SECTION 2 - ENGINEERING DATA

2.1 DESIGN

Information reviewed for the preparation of this report included File 58-11 of the Pennsylvania Department of Environmental Resources (PennDER) and the Pennsylvania Fish Commission's file for the dam. These files contained the following information.

- The earliest correspondence regarding this dam consisted of a dam inspection report by the Water Supply Commission of Pennsylvania, dated 22 May 1920
- 2) The latest dam inspection was conducted on 15 September 1965 by PennDER. They stated that the dam was in good condition except for the accumulation of debris in the spillway and downstream channel.

2.2 CONSTRUCTION

It is not known when the dam was constructed or who performed the original design and construction of the dam. The only information available concerning the construction history of the dam was obtained from the PennDER file on the dam. The information indicated that on 12 April 1938, the dam was inspected by the Water and Power Resources Board, at which time it was in ruins. The dam was then rebuilt in 1939 by the Susquehanna County Sportsmen's Association.

2.3 OPERATION

Maintenance and operations records are now kept by Mr. Chuck Rupert of the Fish Commission. The spillway is uncontrolled and the reservior level is normally at the spillway crest. The dam is visited once a month during the late fall and winter, and approximately every other week or more frequently during the spring, summer and early fall.

2.4 EVALUATION

a. Availability - Other than the information contained in PennDER's File No. 58-11 and the Pennsylvania Fish Commission file for this dam, no design or construction data are available.

- b. Adequacy The information available is generally adequate for a Phase I Inspection.
- c. Validity There is no indication at the present time to doubt the validity of the available engineering data.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

- a. General The dam was found to be in fair overall condition at the time of inspection on 27 October 1980. No unusual weather conditions were experienced during the inspection. Noteworthy deficiencies observed during the visual inspection are described briefly in the following paragraphs. The complete visual inspection checklist, field sketch, top of dam profile, and typical crosssection are given in Appendix A.
- b. Dam An erosion gully was observed at the right downstream abutment of the dam. No other significant problems were observed.
- c. Appurtenant Structures Some debris and sediment has accumulated in the spillway approach channel.
- d. Reservoir Area The reservoir slopes are mild to moderate with no signs of instability. Two dams are located upstream of Purdy Dam. Both of these have been inspected by Michael Baker, Jr., Inc. and their Phase I Inspecton Reports are currently being prepared. These two dams are Page's Lake Dam (NDI No. PA 00062, PennDER No. 58-5) and Fuller's Lake Dam (NDI No. PA 00073, PennDER No. 58-121).
- e. <u>Downstream Channel</u> The downstream channel is crossed approximately 1.5 miles downstream by a bridge carrying PA Route 492. One trailer and two homes are located downstream of the dam. They may suffer economic damage if the dam should fail.

SECTION 4 - OPERATIONAL PROCEDURES

4.1 PROCEDURES

There are no formal written instructions for lowering the reservoir or evacuating the downstream area in case of an impending failure of the dam.

It is recommended that formal emergency procedures be adopted, prominently displayed, and furnished to all operating personnel.

4.2 MAINTENANCE OF DAM AND APPURTENANCES

The Pennsylvania Fish Commission is responsible for the maintenance of the dam. Generally, the maintenance procedures followed by their personnel are considered adequate.

The accumulation of debris and sediment should be removed from the approach channel to the spillway.

4.3 MAINTENANCE OF OPERATING FACILITIES

There are no operating facilities for the dam. An emergency drawdown plan should be developed in case an emergency drawdown should become necessary.

4.4 DESCRIPTION OF ANY WARNING SYSTEM

There is no warning system in the event of a dam failure. An emergency warning system should be developed.

4.5 EVALUATION OF OPERATIONAL ADEQUACY

The current operational features are adequate for the purpose they serve. However, it is recommended that a formal maintenance and operations manual be prepared for the dam.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 EVALUATION OF FEATURES

- a. <u>Design Data</u> No hydrologic or hydraulic design calculations are available for Purdy Dam.
- b. Experience Data The maximum flood of record was reported to have occurred during the winter of 1977. At this time the depth of flow in the spillway was reported to have been 1.5 feet. This corresponds to a flow of 115 c.f.s.
- c. <u>Visual Observations</u> During the visual inspection, no problems were observed which would indicate that the dam and appurtenant facilities could not perform satisfactorily during a flood event.

There is one low spot on the dam crest (Station 1+10) which is only 0.6 feet above the spillway crest.

Page's Lake Dam (NDI No. 00062) is 2050 feet upstream from Purdy Pond. Page's Lake Dam is a 162 feet long, 15 feet high, dry masonry dam with a concrete spillway 40 feet wide by 4.5 feet high.

Fuller's Lake Dam (NDI No. 00073) is 9300 feet upstream from Page's Lake. Fuller's Lake Dam is a 143 feet long, 9 feet high, earthfill dam with a trapezoidal earth spillway.

d. Overtopping Potential - Purdy Dam is a "Small" size - "Significant" hazard dam requiring evaluation for a spillway design flood (SDF) in the range of the 100-year flood to the 1/2 Probable Maximum Flood (1/2 PMF). Because the dam is on the low end of the "Small" size category in terms of height and storage capacity, the 100-year flood was chosen as the SDF.

Using material from "The Hydrologic Study - Tropical Storm Agnes" prepared by the Special Studies Branch, Planning Division, North Atlantic Division, Corps of Engineers, in New York City, December 1975, the peak inflow to the impoundment for the 100-year flood was calculated to be 1595 c.f.s.

The hydraulic characteristics of the basin, specifically, the Snyder's unit hydrograph parameters, were obtained form a regionalized analysis conducted by the Baltimore District of the U.S. Army

Corps of Engineers. Using zero as an initial and constant loss rate, a flow of only 1170 c.f.s. was obtained; therefore, the SCS dimensionless unit hydrograph approach was used to obtain the 100-year flood hydrograph.

The hydraulic capacity of the dam, reservoir, and spillway was then assessed by utilizing the U.S. Army Corps of Engineers' Flood Hydrograph Package, HEC-1 DB. The hydrograph from Fuller's Lake Dam (NDI No. PA 00073) was routed downstream to Page's Lake Dam (NDI No. PA 00062) and combined with the runoff hydrograph for Page's Lake. It was then routed through Page's Lake Dam, downstream to Purdy Dam and combined with the runoff hydrograph for Purdy Pond.

Analyses of the dam and spillway show that Purdy Dam will be overtopped by a maximum depth of 4.32 feet for a total duration of 40.83 hours.

e. Spillway Adequacy - As outlined in the above analyses, the spillway will not pass the SDF without overtopping the dam; therefore, the spillway is considered "Inadequate."

SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

- a. <u>Visual Observations</u> There were no structural inadequacies noted during the visual inspection that cause concern for the structural stability of the dam.
- b. Design and Construction Data - No design or construction data were available for review. Generally, for this type of dam, if the ratio of the width of the stonewall portion of the dam is greater than 0.5 times the height of the dam (w/h), then stability of the dam due to overturning or sliding is not a problem. (Reference "Evaluation and Repair of Stonewall-earth Dams," by Kent A. Healy, Proceedings of "Safety of Small Dams," New England College, Henniker, New Hampshire, August 4-9, 1974, pp 149-178). The w/h ratio for this dam is close to one and no sign of instability was observed during the visual inspection, therefore, further assessments of the structural stability are not considered necessary.
- c. Operating Records No operating records are available. Nothing in the procedures described by the owner's representative indicates concern for the structural stability of the dam.
- d. <u>Post-Construction Changes</u> No changes adversely affecting the structural stability of the dam have been performed.
- e. Seismic Stability The dam is located in Seismic Zone 1 of the "Seismic Zone Map of the Contiguous United States," Figure 1, page D-30, "Recommended Guidelines for Safety Inspection of Dams." This is a zone of minor seismic activity; therefore, further consideration of the seismic stability is not warranted.

7.1 DAM ASSESSMENT

- a. Safety Purdy Dam was found to be in fair overall condition at the time of inspection. Purdy Dam is a "Significant" hazard "Small" size dam requiring a spillway capacity in the range of the 100-year flood to the 1/2 PMF. Because Purdy Dam is on the low end of the "Small" size category in terms of height and storage capacity, the 100-year flood was chosen as the SDF. As presented in Section 5, the spillway and reservoir are not capable of passing the 100-year flood without overtopping the dam. During the 100-year flood, the dam is overtopped by a maximum depth of 4.32 feet for a total duration of 40.83 hours. Therefore, the spillway is considered "Inadequate."
- b. Adequacy of Information The information available and the observations made during the visual inspection are considered sufficient for a Phase I Inspection Report.
- c. <u>Urgency</u> The owner should immediately initiate the further evaluation discussed in paragraph 7.1.d.
- d. Necessity for Additional Data/Evaluation The hydraulic/hydrologic analysis performed in connection with this Phase I Inspection Report has indicated the need for additional spillway capacity. It is recommended that the owner immediately initiate an engineering study to further evaluate the spillway capacity and develop recommendations for remedial measures to reduce the overtopping potential of the dam.

7.2 RECOMMENDATIONS/REMEDIAL MEASURES

The inspection revealed certain items of remedial work which should be performed by the owner without delay. Item I below should be completed by a qualified professional engineer experienced in the design of hydraulic structures for dams. These include:

1) Initiate an engineering study to further evaluate the spillway capacity and develop recommendations for remedial measures to reduce the overtopping potential of the dam.

- 2) Fill the erosion gully at the right downstream abutment of the dam and reseed the area.
- 3) Remove the debris and silt at the entrance to the spillway.
- 4) Provide means to draw down reservoir during an emergency.

In addition, the following operational measures are recommended to be undertaken by the owner:

- Develop a detailed emergency operation and warning system.
- 2) During periods of unusually heavy rain, provide around-the-clock surveillance of the dam.
- When warning of a storm of major proportions is given by the National Weather Service, activate the emergency operation and warning system.

It is further recommended that formal inspection, maintenance, and operation procedures and records be developed and implemented. An emergency drawdown plan should be developed in case an emergency drawdown should become necessary. These should be included in a formal maintenance and operations manual for the dam.

APPENDIX A

VISUAL INSPECTION CHECK LIST, FIELD SKETCH, TOP OF DAM PROFILE, AND TYPICAL CROSS-SECTION

Check List Visual Inspection Phase 1

M.S.L. Coordinates Lat. N 41°51.7' Long. W 75°40' Tailwater at Time of Inspection ft.* Temperature Weather Partly Cloudy County Susquehanna State PA M.S.L. 1409.0 ft.* Date of Inspection 27 October 1980 Pool Elevation at Time of Inspection Name of Dam Purdy (Stump Pond) Dam NDI # PA 00063 PennDER #58-11

Inspection Personnel:

Michael Baker, Jr., Inc.:

*Assumed elevation from U.S.G.S. 7.5 minute topographic quadrangle, Harford, Pennsylvania.

James G. Ulinski Wayne D. Lasch Jeffrey S. Maze

Owner's Representatives:

Mr. E. Grindall Charles J. Rupert Pennsylvania Fish Commission, Division of Fisheries and Engineering

James G. Ulinski

Recorder

MASONRY DAMS

Name of Dam: PURDY DAM

NDI # PA 00063

REMARKS OR RECOMMENDATIONS OBSERVATIONS VISUAL EXAMINATION OF

LEAKAGE

None observed

STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS

Slight erosion along right downstream abutment.

ght downstream Fill in gully and seed area.

DRAINS

None observed

WATER PASSAGES

None observed

FOUNDATION

No problems observed

MASONRY DAMS

Name of Dam: PURDY DAM NDI # PA 00063 VISUAL EXAMINATION OF	OBSERVATIONS REMARKS OR RECOMMENDATIONS	OMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	None observed	
STRUCTURAL CRACKING	None observed	
VERTICAL AND HORIZONTAL ALIGNMENT	No problems observed	
MONOLITH JOINTS	Not Applicable	
CONSTRUCTION JOINTS	Not Applicable	

EMBANKMENT - Not Applicable

Name of Dam PURDY DAM

NDI # PA 00063

VISUAL EXAMINATION OF OBSERVATIONS

REMARKS OR RECOMMENDATIONS

SURFACE CRACKS

UNUSUAL MOVEMENT OR CRACKING AT OR BEYOND THE TOE SLOUGHING OR EROSION OF EMBANKMENT AND ABUTMENT SLOPES REMARKS OR RECOMMENDATIONS

EMBANKMENT - Not Applicable

Name of Dam PURDY DAM

NDI # PA 00063

VISUAL EXAMINATION OF

OBSERVATIONS

VERTICAL AND HORIZONTAL ALIGNMENT OF THE CREST

RIPRAP FAILURES

EMBANKMENT - Not Applicable

Name of Dam PURDY DAM

NDI # PA 00063		
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
JUNCTION OF EMBANKMENT AND ABUTMENT, SPILLWAY AND DAM		
ANY NOTICEABLE SEEPAGE		
STAFF GAGE AND RECORDER		
DRAINS		

OUTLET WORKS - Not Applicable

NDI # PA 00063		
VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT		
INTAKE STRUCTURE		
OUTLET STRUCTURE		
OUTLET CHANNEL		

EMERGENCY GATE

UNGATED SPILLWAY

		REMARKS OR RECOMMENDATIONS
		OBSERVATIONS
Name of Dam: PURDY DAM	NDI # PA 00063	VISUAL EXAMINATION OF

Not Applicable

CONCRETE WEIR

Remove debris and sediment. Accumulation of debris and sediment. APPROACH CHANNEL

Good condition. DISCHARGE CHANNEL

None observed BRIDGE AND PIERS

0	,
_	4
~	ï
-	:
;	:
•	'
•-	!
7	!
Š	1
	Ļ
Annlicable	ï
NO.	١
C)
õ	٠
_	٠
ŧ	
•	
>	
2	
2 417	
Think	
TIME	1 17 14 17
TITIME	
DILILIAN	
COTITION	
VAULTITUD COURS	

		REMARKS OR RECOMMENDATIONS						
		OBSERVATIONS			•			
Name of Dam: PURDY DAM	NDI # PA 00063	VISUAL EXAMINATION OF	CONCRETE SILL	APPROACH CHANNEL		DISCHARGE CHANNEL	BRIDGE AND PIERS	

GATES AND OPERATION EQUIPMENT

INSTRUMENTATION

Name of Dam: PURDY DAM	
NDI # PA 00063	
VISUAL EXAMINATION	OBSERVATIONS REMARKS OR RECOMMENDATIONS
monumentation/surveys	None observed
OBSERVATION WELLS	None observed
WEIRS	None observed
Piezometers	None observed

OTHER

REMARKS OR RECOMMENDATIONS

RESERVOIR

Name of Dam: PURDY DAM

NDI # PA 00063

VISUAL EXAMINATION OF OBSERVATIONS

SLOPES

The reservoir slopes are gentle to moderate with no signs of instability. PA Route 492 is on the right reservoir shoreline.

SEDIMENTATION

The upper fifth of the reservoir is silted in. This sedimentation problem should not significantly affect the performance of the dam and reservoir during flood events.

UPSTREAM DAMS

- Page's Lake Dam (NDI # PA 00062, PennDER
 # 58-5) is upstream of Purdy Dam. A
 Phase I Inspection Report is being prepared by Michael Baker, Jr., Inc. concurrently with this inspection report.
- 2) Fuller's Lake Dam (NDI # PA 00073, PennDER # 58-121) is located upstream of both Purdy Dam and Page's Lake Dam. A Phase I Inspection Report for this dam is also in the process of preparation.

DOWNSTREAM CHANNEL

Name of Dam: PURDY DAM

NDI # PA 00063

VISUAL EXAMINATION OF

CONDITION (OBSTRUCTIONS, DEBRIS, ETC.)

Some vegetation is present in the downstream channel but no debris or blockages are present.

OBSERVATIONS

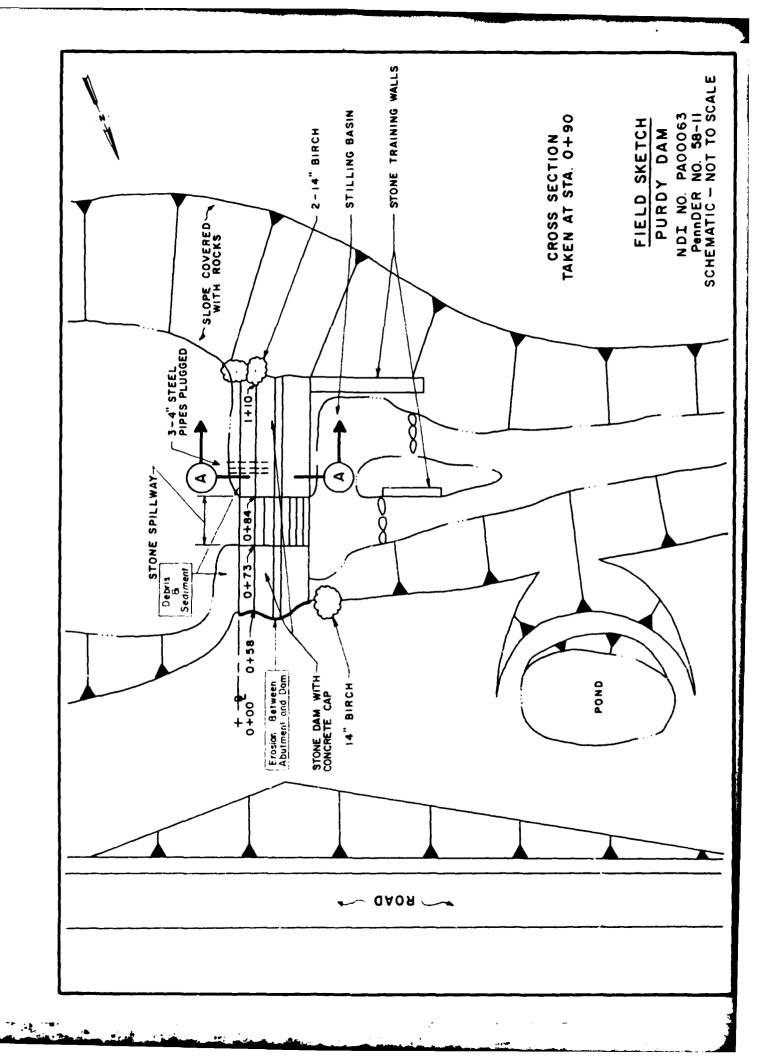
REMARKS OR RECOMMENDATIONS

SLOPES

The downstream channel slope is moderate. The side slopes are well-vegetated and no problems were observed.

APPROXIMATE NO. OF HOMES AND POPULATION

A bridge carrying PA Route 492 over the channel is located downstream. This bridge has an opening 13 ft. wide by 5 ft. high. One trailer and 2 homes are located downstream of this bridge.



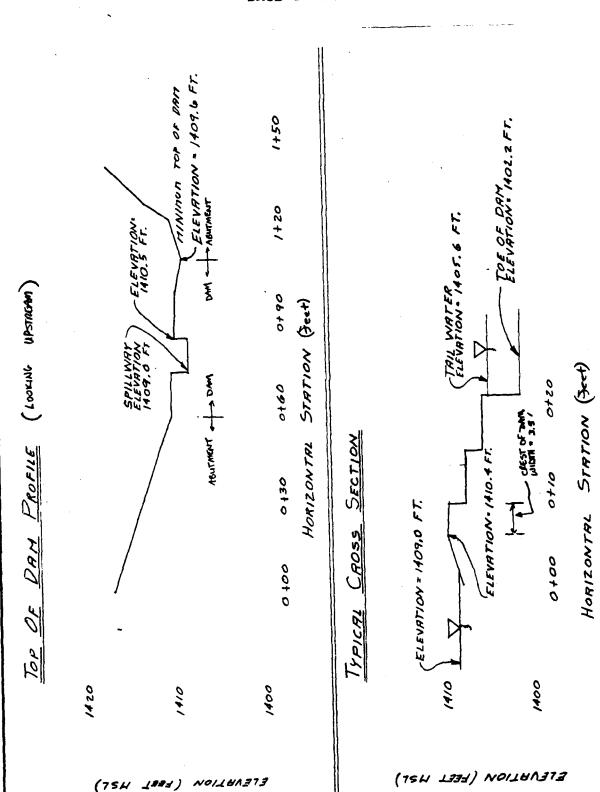
MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

Box 280 Beaver, Pa. 15009 PURDY (STUMP POND) DAM

TOP OF DAM PROFILE TYPICAL CROSS-SECTION

DATE OF INSPECTION: 27 October 1980



APPENDIX B

ENGINEERING DATA CHECK LIST

CHECK LIST ENGINEERING DATA DESIGN, CONSTRUCTION, OPERATION

Name of Dam: PURDY DAM

NDI # PA 00063

TTEN

PLAN OF DAM

REMARKS

None available

REGIONAL VICINITY MAP

A USGS 7.5 minute topographic quadrangle, Harford, Pennsylvania, was used to prepare the vicinity map which is enclosed in this report as the Location Plan (Plate 1).

No dates or construction history is known.

TYPICAL SECTIONS OF DAM

CONSTRUCTION HISTORY

No information available

HYDROLOGIC/HYDRAULIC DATA

No information available

OUTLETS - PLAN

No information available

- DETAILS

No information available

No information available

- CONSTRAINTS

No information available

- DISCHARGE RATINGS

None available

RAINFALL/RESERVOIR RECORDS

PURDY DAM Name of Dam:

NDI # PA 00063

TTEH

REMARKS

DESIGN REPORTS

No information available

GEOLOGY REPORTS

No information available. The regional geology is presented as Appendix F of this report.

No information available

HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES DESIGN COMPUTATIONS

No information available

MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY FIELD

None POST-CONSTRUCTION SURVEYS OF DAM

BORROW SOURCES

No information available

Name of Dam: PURDY DAM

NDI # PA 00063

ITEM

REMARKS

MONITORING SYSTEMS

None

MODIFICATIONS

Dam was reconstructed in 1939 by the Susquehanna Sportsmen's Association

HIGH POOL RECORDS

No information available

POST-CONSTRUCTION ENGINEERING STUDIES AND REPORTS

No detailed engineering report other than the 22 May 1920 Water Supply Commission Inspection is available. A number of inspection reports are available in the PennDER file, including the latest recorded inspection on 15 October 1965 by PennDER.

PRIOR ACCIDENTS OR FAILURE OF DAM NO DESCRIPTION

REPORTS

None reported in the information available.

MAINTENANCE OPERATION RECORDS

Formal records of maintenance are kept by the Pennsylvania Fish Commission.

Name of Dam: PURDY DAM

NDI # PA 00063

ITEM

No information available

SECTIONS, and DETAILS SPILLWAY PLAN,

No information available OPERATING EQUIPMENT PLANS & DETAILS

CHECK LIST HYDROLOGIC AND HYDRAULIC DATA ENGINEERING DATA

DRAINAGE A	REA CHARACTERISTICS: 6.63 sq.mi., mild to steep slopes
	with wooded areas.
ELEVATION S	TOP NORMAL POOL (STORAGE CAPACITY): 1409.0 ft.
	(54 acft.)
ELEVATION !	TOP FLOOD CONTROL POOL (STORAGE CAPACITY): 1409.6 ft.
	(62 acft.)
ELEVATION I	MAXIMUM DESIGN POOL:Unknown
ELEVATION :	TOP DAM: 1409.6 ft. (minimum crest elevation)
SPILLWAY:	
b. 5	Crest Elevation 1409.0 ft. Type Broad crested masonry weir Width of Crest Parallel to Flow 3.5 ft.
d. 1	Length of Crest Perpendicular to Flow
e. 1 f. 1	Location Spillover Center of dam Number and Type of Gates None
OUTLET WORK	KS: None
	Type
	Location
d. 1	Entrance Inverts Exit Inverts
	Emergency Drawdown Facilities
HYDROMETEO	ROLOGICAL GAGES: None
a. :	lype
	Location
c. I	Records
MAXIMUM NO	N-DAMAGING DISCHARGE 115 c.f.s.

APPENDIX C

PHOTOGRAPH LOCATION PLAN AND PHOTOGRAPHS

DETAILED PHOTOGRAPH DESCRIPTIONS

Overall View of Dam

Photograph Location Plan

Photo 1 - View of Upstream Side of Dam from Right Shoreline

Photo 2 - View of Upstream Side of Dam from Left Shoreline

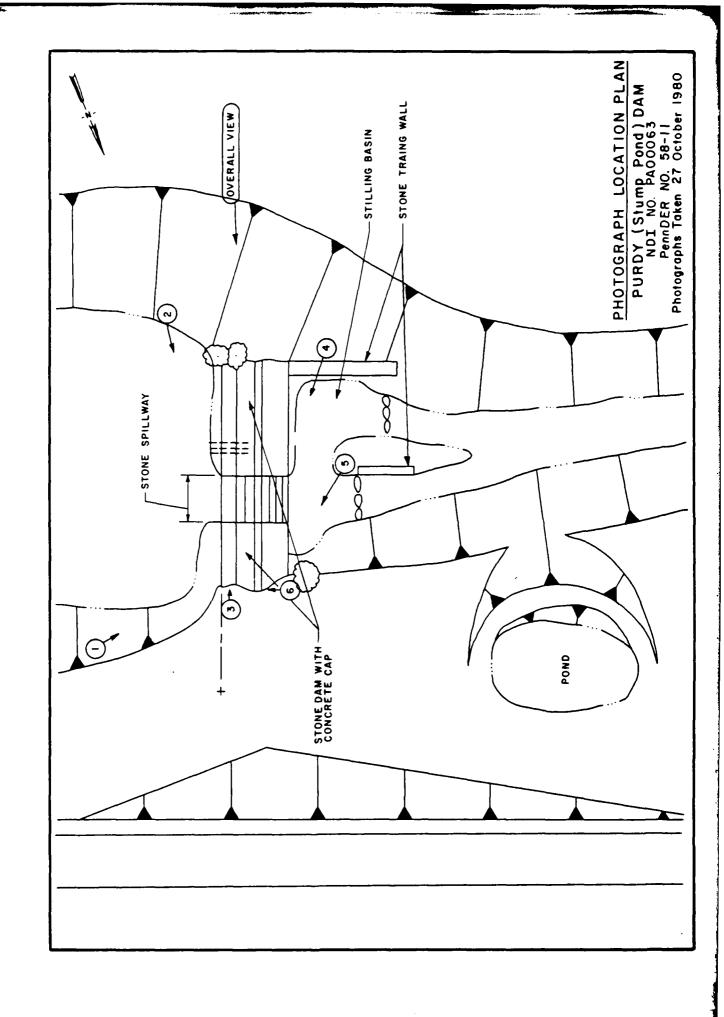
Photo 3 - View Across Crest of Dam from Right Abutment

Photo 4 - View of Downstream Side of Dam from Left Abutment

Photo 5 - View of Right Abutment

Photo 6 - Eroded Area of Right Abutment

Note: Photographs were taken on 27 October 1980.



PURDY (STUMP POND) DAM



PHOTO 1. View of Upstream Side of Dam from Right Shoreline



PHOTO 2. View of Upstream Side of Dam from Left Shoreline

PURDY (STUMP POND) DAM



PHOTO 3. View Across Crest of Dam from Right Abutment

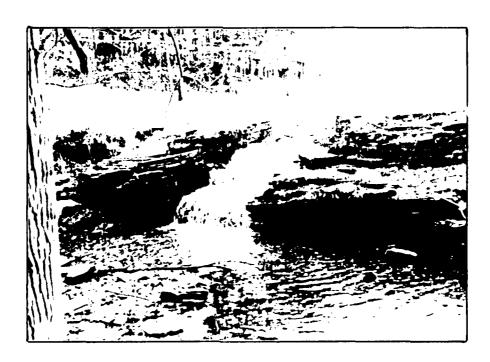


PHOTO 4. View of Downstream Side of Dam from Left Abutment

PURDY (STUMP POND) DAM

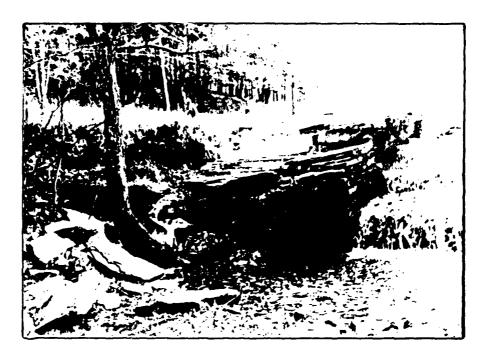


PHOTO 5. View of Right Abutment



PHOTO 6. Eroded Area of Right Abutment

APPENDIX D

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

MICHAEL BAKER, JR., INC	
THE BAKER ENGINEERS	

Beaver, Pa. 15009

Box 280

Subject PURE	Y DAM		S.O. No
APPENDIX	D- HYDROLOGIC	AND	Sheet No of
	COMPUTATIONS		
Computed by	Checked by		Date

SUBJECT	PAGE
Prefre	i
HYDROLOGY AND HYDRAULIC DATA BASE	1
HYDRAULIC DATA	2
DRAINAGE AREA AND CENTROID MAP	3
TOP OF DAM PROFILE AND CROSS SECTION	4
SPILLWAY DISCHARGE RATING	5
100-YEAR STORM DISTRIBUTION	6
100-YEAR DISCHARGE CALCULATION	7
ROUTING SUMMARY	10
HEC-I CAPACITY ANALYSIS	//

PREFACE

HYDROLOGIC AND HYDRAULIC COMPUTATIONS

The conclusions presented pertain to present conditions, and the effect of future development on the hydrology has not been considered.

PYDLOLOGY AND A YUMANI IC ANALYSIS I VIA BANI

MASSE OF TIME PURES LAM

100-YEAR STURM * the Inches. 14 hours *

STATION	1	2	3	i.	
Station besitaption	FULLER'S LAKE DAM NDI F PA JOUTS	PAGE'S LAKE DAM NII 6 FA 00061	PURDY DAM NDI # PA 00065		
ininace Area (square miles)	0.45	z.83	1.85		
Cumulative Drainage Area (square miles)	0.95	u.78	6.63		
Adjustment of PMF (for Drainage Area (1)					
t Bours 12 Bours 20 Bours 08 Bours 72 Bours	100-YEAR STORM DISTRIBUTION ON SHEET 6	100-YEAR STORM DISTRIBUTION ON SHEET 6	100-YEAR STORM DISTRIBUTION ON SHEET 6		
SCS Dimensionless Unit Hydrograph Parameters	T = 1.36 hr.	T _c = 2.07 hr.	T = 1.32 hr.		
	Lag Time = .82 hr.	Lag Time = 1.24 hr.	Lag Time = 0.79 hr.		
	CN = 70	CN = 64	CN = 71		

Spillway Data
Crest Length (ft)
Freeboard (ft)
Discharge Coefficient
Laponent

TRAPEZOIDAL SPILLWAY SPILLWAY RATING RATING CURVE TAKEN CURVE TAKEN RATING CURVE FROM FULLER'S LAKE FROM PAGE'S DEVELOPED ON SHEET 5

⁽¹⁾ Technical Paper No. 40, Cooperative Studies Section, U.S. Weather Bureau, Washington, D.C., 1961.

MICHAEL BAKER JR. INC. not e. 1 Steen No. 2 2 23 THE NAKER ENGINEERS Drawing No 18 6 28 with the execution of the love of the second ಎಂ. 10 ನ ಕ Bruch of Burn School Commence of the contract of th Constitution of the property of MAY A CONTRACT 4 - 0 ٠- ا د ∼ خباد ∘ بساحبر The state of the s Programme Appendix THE STATE OF STATE OF THE STATE 1 ÷c. D. G. PROSE REPORT OF THE P. P. H. LE. ELT MATER FALL GIERNIS JETTA 242 SECTION 6 48 SEC. 1-01-A. 10- -- 1741 - 1/2 - 1/3 (1.94 + 1-1/41) 3 16 = 54.20 & FT. THE OF LAW STORAGE 32 40-FT FAM HES 412-455 SNOOPS WART HYCKEGIANH "MIGHETERS L= 299 17., - 200 1 / 36 1/2. NATERSHED IS IN ZONE I A C. 150 , C, 0.62 To: 150 (6 x Lea) " > 2.28 DRAINAGE AREA HOOVE DAM - 6.63 SO M.

CHAEL BAKER, JR., INC.	Subject PUA					337-00-AA
THE BAKER ENGINEERS	TOP OF	DAM	PROFILE		_ Sheet No	4_ of <u>23</u>
Box 280			SECTION		_ Drawing No.	
Beaver, Pa. 15009	Computed by _	GWI	Checked by	WDL	Date _//-	17-80
0 00 00	ABUTMENT ON - FLEVATION - 1409, LO FT. 1400	0 too 0 tso 0 tso 1 tso		V-1410.4 FT.	1400 0+00 0+10 0+20	HORIZONTAL STATION (Sect)

MICHAEL BAKER, JR., INC.

THE BAKER ENGINEERS

Subject PURDY DAM S.O. No. 13837-00-ARA-04

SPILLUAY DISCHARGE RATING Sheet No. 5 of 23

Box 280 Beaver, Pa. 15009 Computed by GWT Checked by WDL Date 11-20-80

SPILLWAY PROFILE

TOP OF SPILLWAY WALL AT ELEV. : 1410.5 FT.

SPILLWAY CREST AT ELEV. : 1409.0 FT.

Z TO | SLOPE

SEDIMENT

ROCK

TO DOWNSTREAM CHANNEL

1400

1410

0+00 0+10 0+20

DEVELOP RATING CURVE BASED UPON CRITICAL FLOW OVER SPILLWAY:

V = \(\sqrt{g} \) \(\text{CHOW}, OPEN CHANNEL HYDRAULICS, P. 43 \)

g = 32.2 FT/SEC. FLOW AREA

D = MERN HYDRAULIC DEPTH = FREE SURFACE TOF WIDTH = T

Y = MEAN FLOW VELOCITY

Q=AV

ELEV.,	FLOW DEPTH,	AREA.	TOPWIDTH,	岑	V. Fig.	Q,CFS	¥29	FGL, FT.
1409.0	0	0	0	0	0	0	0	1409.0
•	0.5	5.5	11	۔ ج	4.01	22.06	0.25	1409.75
1409.5	1	11.0	11	1.0	5.67	62.37	0.50	1410.50
1410.0	1.0		1//	1.5	6.95	114.67	0.75	1411. 25
1410.5	1.5	16.5	1	7.0	8.03	176.66	1.00	1412.00
1411.0	2.0	22.0	///	2.5	8.97	246.67	1. 2.5	1412.75
1411.5	2,50	27.5	//		1	3 24.34	}	1413.50
1412,0	7.0	33.0	//	7.0	9.83	}	1	1415.00
1413.0	4.0	44.0	//	4.0	11.35	499.40)	1416.50
1414 0	50	55.0	11	5.0	12.69	697,87	12,50	1716,70

CHAEL BAKER, JR., INC.	Subject PURDY			.O. No	
THE BAKER ENGINEERS	100 - YEAR	STORM D	SISTRIBUTION S	heet No. <u>6</u> of _	23
Box 280	**************************************			Drawing No.	
Box 280 Beaver, Pa. 15009	Computed byG_C	UTChecke			
,	C 6pc.toc 5/		• • • • • • • • • • • • • • • • • • • •	, or	
2.0			2.0		
100 -	YEAR		e centro e e colonia do la la colonia de la		
RAINF	ALL AMOUNTS FRE	ON			
The second s	TP-40:				
/// T	IN. 2.0 /A				
J.HR.		\$ L			
ZHR		·			-,
3. HA	7.5.7~	~ = = =			
V	4.4 1A				
5_1.0 + 12 HA	P. 3 -/~	<u></u>			
N 24_H	8 6.2 /A				
8					
3					
8		0.5			
0,5			0.35		
			للرائية المستوجة بالأقال المراجعة		
			0,15		
a part of a management of the second of the			CO. 15 0.075		
			L		
			50.0	37	
			70.0	37	
0 Z 4	6 8 10 12	1	60.0	37	
0 2 4	6 B 10 12	1	60.0	24.	
0 2 4		1	60.0	24	
O Z 4		1	60.0	24.	4
RAINFALL	DISTRIBUTION	1	60.0	24.	
	DISTRIBUTION TE INTERVALS	85. DN	15 20 22	24	
	DISTRIBUTION INTERVALS	85. DN	60.0	24	RVA
	DISTRIBUTION TE INTERVALS	85. DN	15 20 22	24	RVA
	DISTRIBUTION TE INTERVALS DE NUMBERS	90 TOTAL RA	15 20 22	24	RVA
	DISTRIBUTION INTERVALS	85. DN	15 20 22	24	RVA
	DISTRIBUTION TE INTERVALS DE NUMBERS	90 TOTAL RA	15 20 22	24	TR VA
	DISTRIBUTION TE INTERVALS DE NUMBERS	96 TOTAL RA	15 20 22	N ERCH INTE	RYA
	DISTRIBUTION TE INTERVALS DE NUMBERS	96 TOTAL RI 0.6 1.2 2.4 2.5 5.7	OCCURING /	N ERCH INTE	T V VA
	DISTRIBUTION TE INTERVALS DE NUMBERS	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	RVA
	DISTRIBUTION TE INTERVALS DE NUMBERS	96 TOTAL RI 0.6 1.2 2.4 2.5 5.7	OCCURING /	N ERCH INTE	* YA
	DISTRIBUTION TE INTERVALS TO 17 THE TO THE T	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	TR VA
	DISTRIBUTION TE INTERVALS DE NUMBERS	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	RYA
	DISTRIBUTION TE INTERVALS TO 17 THE TO THE T	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	RYA
	DISTRIBUTION TE INTERVALS TO 17 THE TO THE T	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	TR VA
	DISTRIBUTION TE INTERVALS TO 17 THE TO THE T	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	RVA
	DISTRIBUTION TE INTERVALS TO 17 THE TO THE T	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	RYA
	DISTRIBUTION TE INTERVALS TO 17 THE TO THE T	85. 90 TOTAL RE 0.6 1.2 2.4 2.5 5.7 8.1 32,3	OCCURING /	N ERCH INTE	TRY VA

MICHAEL BAKER, JR., INC.

Subject PART DAM S.O. No.

THE BAKER ENGINEERS

Box 280

Beaver, Pa. 15009

THE INFLOW TO THE IMPOUNDMENT FOR THE 100-YERE FLOOR

THE INFLOW TO THE IMPOUNDMENT FOR THE 100-YEAR FLOOD WAS CALCULATED USING MATERIAL FROM "THE HYPROLOGIC STUDY-TROPICAL STORM AGNES" PREPARED BY THE SPECIAL STUDIES BRANCH, PLANNING DIVISION, NORTH ATLANTIC DIVISION, CORPS OF ENGINEERS, IN NEW YORK CITY.

DRAINAGE AREA - 1.85 Sq. Mi.

O COMPUTE THE MEAN LOGARITHM

LOG(Qm) = Cm + 0.75 LOGA

LOG (Q.) = MEAN LOGARITHN OF ANNUAL FLOOD PEAKS
A: DRAINAGE AREA, Sq. Ti., = 1.85 Sq. Ti.

Cm = MAP COEFFICIENT FOR MEAN LOG OF ANNUAL
PEAKS FROM FIG. 21 = 2.16

LOG (9m) = 2.16 + 0.75 (LOG 1.85) = 2.360

2 COMPUTE STANDARD DEVIATION

5 = Cs - 0.05 (LOG A)

S = STANDARD DEVIATION OF THE LOGARITHMS OF THE ANNUAL PEAKS.

C; = MAP COEFFICIENT FOR STANDARD DEVIATION FROM
FIG. ZZ = 0.35

A : DRAINAGE AREA, SQ. MI. + 1.85 Sq. 171.

S = C, -0.05 (LOGA)

: 0.35-0.05 (604 1.85)

= 0,337

- 3 SELECT SKEW COEFFICIENT FROM FIG. 23 = 0,23
- 1 209 (9,00) = 209 (9m) + K(P,9) 5

K(P,): STANDARD DEVIATE FOR A GIVEN EXCEEDENCE FREQUENCY PERCENTAGE (P) AND SKEW COEFFICIENT (g) FROM EXHIBIT 39 OF BEARD'S "STATISTICAL METHODS IN HYDROLOGY"

206 (9100): 209 (9m) + K (P,g) 5 : 2.360 + 2.501 (0.337)

9,00 = 1,595 CFS

USING ZERO LOSS RATES, A PEAK FLOW OF 1170 CFS WAS
OBTAINED IN THE HEC-I ANALYSIS IF THE SNYDERS UNIT
HYDROGRAPH PARAMETERS OKIGINALLY DERIVED FOR THIS
BASIN WERE USED.

MICHAEL BAKER, JR., INC.

Subject PURBY DAM

S.O. No.

THE BAKER ENGINEERS

100 - YEAR DISCHAREE

Sheet No. 8 of 23

CALCULATION 5 (CONTINUED)

Drowing No.

Beaver, Pa. 15009

Computed by GWT Checked by WDL

Date 12-1-80

THE 100-YEAR HYDROGRAPH IS THEREFORE COMPUTED USING THE SCS PIMENSIONLESS UNIT HYPROGRAPH APPROACH. TIME OF CONCENTRATION AND LAG TIME ARE COMPUTED AS FOLLOWS:

To = TIME OF CONCENTRATION = CVERLAND FLOW

TIME + CHANNEL

FLOW TIME

OVERLAND FLOW TIME:

DISTANCE = 4950 FT. 5LOPE = 1800-1920 = 7.7 %

AVERACE FLOW VELOCITY = 0.70 FT/SEC.

(FROM FIG. 3.1, T.R. NO. 55, URBAN HYDROLOGY

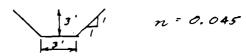
FOR SMALL WATERSHEDS, SCS.)

TRAVEL TIME : 7071 SEC.

CHANNEL FLOW TIME

DISTANCE = 2050 FT. SLOPE = 1720-1410 = 0.49%

ASSUME AVERAGE CHANNEL SIZE IS:



AVERACE FLOW VELOCITY = V = 1.49 R3/3 5/2

V = 1.49 (313) (313) (0.0049) 1/2

V = 2.03 FT/SEC.

TRAVEL TIME : 1010 SEC.

MICHAEL BAKER, JR., INC.

Subject PURPY DAM S.O. No.

THE BAKER ENGINEERS

100-YEAR PIECHARSE Sheet No. 9 of 23

Box 280 Beaver, Pa. 15009 CALCULATIONS (CONTINUED) Drowing No. Computed by Gar T Checked by WAL Date 12-1-80

TOTAL TRAVEL TIME = To = 7071 + 1010 = 8081 SEC. = 2,24 HR.

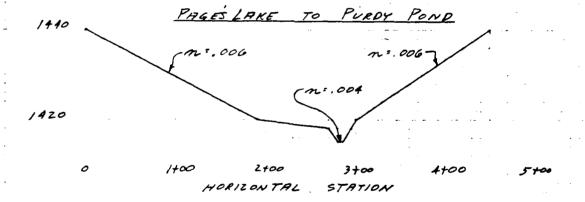
LAG TIME = 0.6 Tc = 1.35 HR.

WITH THE SCS PROCEPURE, A CURVE NUMBER OF 68
PRODUCED A PEAK FLOW OF 1580 CFS THIS VALUE 15 WITHIN I % OF THE PREVIOUSLY COMPUTED PEAK FLOW OF 1595, 3 CFS AND IS WITHIN THE 10 % LIMIT SUGGESTED BY THE CORPS GUIDELINES.

		= .	
MICHAEL BAKER, JR., INC.	Subject PURDY DAM	S.O. No	
THE BAKER ENGINEERS	ROUTING SUNDARY	Sheet No	10 01 23
Box 280		Drawing No	
Beaver, Pa. 15009	Computed by <u>GUT</u> Checked I	by Date <u>/-2</u>	0-81
1			

NAME	LENGTH OF DAM	HEIGHT OF	NORITAL POOL STORAGE	TOP OF DAM STORAGE	ROUTING LENGTH OF CHANNEL
PURDY POND	52 Fr.	7.4 Fr.	54. Z RC-FT, 1409. O FT	62 Ac,-Fr. 1409.6 FT.	
PAGE LAKE	162 Fr.	15 Fr.	971. / Ac-FT 1433, O FT.	1431 Ac-Fr 1436. Z Fr.	2050 FT.
FULLER LAKE	143 Fr.	9 Fr.	60,7 Ac.Fr. 1537.0 Fr.	114 Re-Fr. 1539.6 FT.	9300 FT.

TYPICAL ROUTING CHANNELS



FULLER'S LAKE TO PAGE'S LAKE

O 1+00 2+00 3+00 HORIZONTAL STATION

1480

// 14 40 U.012 U.012 U.012 U.012 0.005 0.012 0.012 Э 0-000 0-012 0-024 0-012 0.012 0.012 0.024 0.012 153 * 0.000 0.012 0.012 0.012 0.012 1480 1543 0.012 0.024 0.024 0.012 0.006 7 NATIONAL PROGRAM FUR INSPECTION OF NON-FEDERAL DAMS
AYJAULDGIC AND HYDRAULIC ANALYSIS OF PORLY DAM
UNIT HYDROGRAPH BY SNYDERS WETHUD

0 0 0 -1537.0 -1540:2 ...1540:3 -045.8 074.1 10:0 0.000 0.000 0.024 0.024 1542.5 0.000 0.024 0.024 0.024 9300 1500 1500 0.006 0.006 0.006 0.024 0.024 0.006 0.024 0.024 0.024 1939:5 1541.5 KOUSTING THRU CHANNEL TO PAGE LAKE 1500 144 350 0.006 0.006 0.002 0.023 0.006 0.006 0.012 0.025 ROJI ING FOR FULLERS LAKE DAM TO PAGE 15.86 1.4.52 18.86 1951 66 1641 1631 1631 0.006 0.006 0.006 0.012 0.031 RUIDEF HYDROGRAPH TO DAM MUJUFF HYDROGRAPH 1938.3 15.0.5 02 00 02 02 02 03 03 04 0.006 0.006 0.012 0.323 0.006 0.95 0.006 0.012 0.323 6:2 1.03c 1.03c 0.012 0.041 29. 15+1 1533 1683 1537:7 3.032 3.032 3.032 3.012 26.0 -0.15 2.030 71 199 V 759 V 759 V 0.032 \$4 13.33 \$2 1535 \$01539.5 410.0 10 610.0 10 610.0 10 610.0 10 710.0 10 \$L 7-\$V1539.0 0.35

្នាស់ទុស - ភេទ្ធិស្នាត្រស់ស្រីស្រែស សេច

1

2.0

-

1
1.53.7 80.2.7 1.53.9
1.13.7 1.13.3.7 1.13.3.7 1.13.3.7 1.13.3.7 1.13.3.7 1.13.3.7 1.13.3.7 1.13.4
1433.7 19.2.35 1433.1 1
1411 113.7 ## 1413.7
##

!					-			Sugar	13 00
					!				
~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	0 - 8 - 0								1
HS AI	A1		1						
KONDIE HYDROGRAPH AL KUUTE HYDROGRAPH TU KUUTE HYDROGRAPH TU RUNDEF HYDROGRAPH AT CUMBINE Z HYDROGRAPHS	ROUTE HYDROGRAPH TO ROUTE HYDROGRAPH TO RUNUFF HYDROGRAPH TO CUMBINE 2 HYDROGRAPHS ROUTE HYDROGRAPHS	END OF NETWORK							
RUNDER HY RUNTE HY RUNDER T	ROUTE RUNUFF CUMBIN	END OF						1	
					1	} !	!		
				:					

LUMP 1033 2223222222 JPRT INAME ISTAGE TAUTO ALSMA RIIMP EXCS LULAL MSTAN KALN I SAME INT END-GF-PERIOD FLUM COMP G HU-UA HK-MW PERIOD ******** SIRIC CNST. RT104 2-00 New Co Ibir Э 70.00 MATLONAL PROGRAM FUR INSPECTION OF NUM-FEDERAL DAMS
TYDICLOSIC AND HYDRAULIC ANALYSIS OF PURDY DAM
ONIT HYDROGORAPH BY SNYDERS METHOU MULTI-PLAN ANALYSES TO BE PERFURMED NPLAN I NRITO" I KRITO" I 8411E TRACE JOB SPECIFICATION
IHR ININ METRO
O 0 0 3
NMT LRUPI TRACE SUB-AREA RUNGEF COMPUTATION JPLT ERAIN SIRKS RIIUK WETNESS = -1.00 EFFECT ON = UNIT HYDRUGRAPH DATA -1.50 URCSN= -0.05 HYDROGRAPH DATA TRSDA TRSPC 0.95 0.0 LRUPI ********* LUSS DATA TECON TAPE SNAP 0.0 RJIUFF HYDRUGRAPH TU DAM LUSS 0 JUPER LUAY L'STAU TOURP 0 1.00 ******** 14KEA 0.95 STRIGE EXCS NHIN 10 -13.00 ULTAR 0.0 MITY 1 JH6 X T CURVE 43 = RILJS= STAKR 40.44 HR.HN PERIUJ DHYD. 0 7004 004 ******** LRUPT 114E 02/17/81 Ş

Z3

304 0.20 2.90 3.24 1124.

******** ******** ********

******** ********

_
7
-
_
-
-
- 3
-
7
À
-
•
0
- 9
d
•
٩
2
-
2
-

1									-			
			1.57.40	1 LUMP	ורכא ם	ITAPE	יים פיים	JPKI	INAME	1 s I A GE	1AU10 0	
		1052	1.0	AVL 0.0	IRES 1	RUUTING DATA RES ISAME	10Pf G	JPMP J		LSIK		
			143 195	NSTOL	LAG	AMSKK J.O	× 2.0	1.0 2.0	STUKA -1551.	15PRAT		
STAGE 15.		337.	15.	1538.30	1539.00		1539.00	1540.20		1540.33		
FLOA	0.0	29.40	F	100.30	01:\$22		370.80	635.80		016.10		
SUNFACE AREA=	14.	17.	•	26.	39.		:		;	!		
CAPACITY=	•	61.		124.	762.							
EL EVATIONE	1533.	1337.		1540.	1560.		-					
		LREL 1337.3	D SPHIU	D.D COUNT	UM EXPM	TO CEEVE	1	COUL CAREA	j	EXPL		
						UAM	AIA					
					TUPEL 1539.6	3.1	3-1 1-5 99-	DAMHID 99.				
CREST LENGTH	.0	1	.91	-62	45.	54.	:	.11.	80	-16		
ELEVATION	1539.0	ļ	1540.0	1540.5	1541.0	1541.5		1542.0	1542.5	1543.0		
PEAK GUTFLUM IS	631.	631. AF TE4E	7.00	OO HOURS								
•			*****						321			
		:			HYDRUGE	HYDREGRAPH RUUTING	.5 .5					
		RAJITAS LIRU		CHANNEL TO PAGE LAKE	PAGE LAK	اإس	i					
			-157AQ	I COMP	TECON	TTAPE O	- JPE1	JPRI 0	INAME ISTAGE	1STAGE 0	TAUIU	
		ALCS3	0.0	AVG	IRES .	IRES ISAHE	TUP I	D DWdT		LSTR		SHE
			157755	MSTOL	EAC 0	AMSKK J.O	¥ 0.0	15K	STURA TSPRAI	T SPRAT		15
MISM AL DEPTH CHANNEL ROUTTH	INEL ROUT	-										0#
						i : :	1	1	1	!		N

RESTH SEL 9330.

CRISS SECTION CJUADIMATES—STAFELEV, STAFELEV—ETC 0.0 1500.00 70.30 1491.00 144.00 1483.00 150.00 1480.30 153.00 1463.30 159.30 1483.00 250.30 1491.00 350.00 1500.00

The second of th

144.05 144.25 144.25 145.66 10.001.11 1450.61 1452.94 1452.9	SI Chace	200	2	2.0	0.0	06.5	33.44	10.711	454.03		0.11.61
	01 181 04			P	N. 9		n n		io p		
1431.00 1436.33 1440.05 1443.54 1450.43 1450.65 1450.42 1450.44 1450.30 1450.31 1450.44 1450.31 1450.45 1450.44 1450.30 1450.31 1450.44 1450.30 1450.31 1450.44 1510.30 1450.31 1450.44 1510.30 1450.44 1450.44 1510.30 1450.44 1450.44 1450.44 1510.30 1450.44 1450.44 1450.44 1610.30 1450.44 1450.44 1450.44 1610.30 1450.44 1450.44 1610.30 1450.44 1450.44 1610.30 1450.44 1450.44 1610.30		000	? ?	0	2 2	80 - ¢ B	904.82	84.8404	11.10401	00.10412	3/408.838
1488.26 1471.79 1473.31 1478.84 1482.37 1485.39 1489.42 1489.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.42 1499.43 1499	STAGE -	[433.00	1+36.13	1440.05	1443.54	1647-10	1450.63	1454-10	1457.68	1401.71	1464.74
15 1484-3 0.0 0.0 0.0 0.0 0.0 0.0		1468.26	1.11.19	1475.31	1478-84	1487.31	1+85-49	1493.45	1455-94	14.00.41	1500.00
13 1384-3	FLUM	0.0	2.0	0.0	0.0	0.0	0.0	0.0	3	3	ריים
SUB-AREA KUNUFF CUMPUTATION SUB-AREA KUNUFF CUMPUTATION R. A.		0.0	?.0	0.0	0.0	69.68	78-496	40.84.4d	10287.11	24404-00	37408.48
SUB-RREA RUNDFF CUMPUTATION SUB-RREA RUNDFF CUMPUTATION SUB-RREA RUNDFF CUMPUTATION SUB-RREA RUNDFF CUMPUTATION SUB-REA RUNDFF RUND	CEMUY STAC	S	•3								
SUB-AREA RUNOFF COAPUTATION (1514) 100P 1ECUN 11APE JP11 JPKT INAME 15TAGE LANID (1514) 100P 1ECUN 11APE JP11 JPKT INAME 15TAGE LANID (1514) 100P 1ECUN 11APE JP11 JPKT INAME LULAL (1514) 100P 1ECUN 11APE JP11 JPKT INAME LULAL (1514) 100P 1ECUN 11APE JP11 JPKT INAME LULAL (1514) 11APE JP 11APE JP 11APE JP11 JPKT INAME LULAL (1514) 11APE JP 11APE	:	*******		******	***	******			***		· · · · · · · · · · · · · · · · · · ·
1814 1000 1100				SUS	-AREA RUNDE	COMPUTATION					
15144 15146 15146 15146 15146 14019 14019 14010 14019 14010 1401		; ;	Ŧ	OGRAPH TU PA	GE LAKE						
IHYDG			§]			Jac		ļ	PAULU 0		
LUSS JAIA LUSS JAIA LUSS JAIA LUSS JAIA LUSS JAIA LUSS STRIC CN-SIL ALSHX RIIHP 0 0-3 0-3 0-0 1.00 0-0 1.00 -1.00 -4.00 0.0 0.0 CURVE 4J = -64.00 0.0 0.0 CURVE 4J = -64.00 0.0 UNIT HYDROGRAPH DAIA TC= 0.0 1AG= 1.24 RELESSIUN JAIA STRTQ= -1.50 GRCSN= -0.05 RIILAR= 2.30 END-UN-PERIOD FLOW RAIN ERCS LUSS COMP 0 HO.DA HR.HN PICKIGD RAIN EACS LUSS COMBINE HYDRUGHAPHS		THY		i					AL		
CURVE 4J = -64.00 WETNESS = -1.00 EFFECT CN = 64.00 1C= 0.0 LAG= 1.24 RECESSION DATA STRTG= -1.50 GRCSN= -0.05 RILURE 2.00 END-OF-PERIOD FLOW HR.MA PERIOD ANTW EXCS LOSS COMP J HO.DA HK.HN PERIOD RAIN EACS LOSS COMBINE HYDROGRAPHS FAUNT STATIONS 3 AND 4 COMBINE HYDROGRAPHS FAUNT STATIONS 3 AND 4			0,0	1.00		RT 10K		ALSHK 0.0	KTIMP 0.0		: ! !
UNIT HYDROGRAPH DATA TC= 0.0		כחמס	9- *	WETNESS	-1:00	FFECT CN =	00.40	1		: : :	
RECESSION DATA STRTG= -1.50 GRCSN= -0.05 RTIOR= 2.00 END-Ut-PERIOD FLOM HR.MA PERIOD RAIN ERCS LUSS COMP G HQ.DA HR.MN PURIOU RAIN ERCS LUSS (12.7) 61.11 90.41 COMBINE HYDRUGHAPHS COMBINE STATIONS 3 AND 4	!			=31	UNIT HYDRO	KAPH DATA					!
HR.MA PERIOJ ALIN EXCS LOSS COHP 3 HG.DA HR.HN PERIOJ RAIN EACS LOSS				1	RECESSION CRCSN	j	RIIJRE 2.00	; ; ; ;			
SUN 6.23 2.41 3.79 1 127.11 01.11 90.11 CUMBINE HYDRUGHAPHS CAMBINE HYDRUGHAPHS CAMBINE HYDRUGHAPHS CAMBINE HYDRUGHAPHS	0 R 3. DA		-	ł		DA	HR.HN PERIC	RAIN	. KCS LUSS -		!
COMBINE HYOROGRAPHS URDGRAPHS FROM STATIONS 3 AND 4	1	. !					ns	6.23	_ m	37036.	
JAOGRAPHS FROM		•	•			•			•		
C. J. J. L. HY JR D. GRAPHS FAUN STATIONS 3 AND 4					COMBINE HYD	HUGRAPHS					
			CYH 3FT& CJ	ROCRAPHS FRO	H STATIONS	AND 4		:			1

•••••• •••••••• •••••••

.

HYDRUGHAPH RUUBING

••••••

••••••

RIJIIII FUR PAUE LAKE UAM

			1,140	LATA ICUMP IECEN ITAPE JPA.I	100 P	IIAPE	141		* 12.	JPRI INAME ISTACE INCIDE	IAUIU		
		1,035	2.0	AV.0	KCGI INES	RCUTING DATA INES ISANC		d H a		* 3			
		i	et PS	ASTOR NSTUL	נאני	LAG AMSKK U U.U	, ,	- ?		51048 13PH41			
STA'se 1483.00		1.13.70		1434-50		1435.20 1436.00	3.0	1431.	5.	02.0441 04.541	1434.00	24.72.20	7 - 7 - 7
FLTW - 0;	C	02:0B	ž	0.0	10:11\$	7 64	1:50	1176.63		CB-9241	1416.00	215.1.23	D2 - B5 5.7
SURFACE AREA=	97.	401	1	.511	274.								
CAPACITYS	3		m.	1936.	6388.								
EL EVATION# 1423. 1733.	1423:	113		1440: 1420:	1460								
		1133	JR11 SP	URLE SPWID LUJM		EXPM ELEVE 0.0		COUL CAREA	Aht A 0.0	0.0			
1		1			TUPEL CUQU 1430.2 3.1	UAN UATA TOGG EX	UATA EXPU	EXPU DAMEIU					
CREST LENGTH	_	•	37.	36	125.	. 185.	5.	197.	203.	. 213.			
	1436	*1 7*	30.5	1437.0	1436-2 1430-5 1437.0 1437.5 1436-0 1436-5	1438	, c.	4,44.5	1434.0	1439.5	^		

PEAK DUTFLOW IS 832. AT 14.4E 9.00 HUDRS

HYDRECKAPH RUJIING

RIJILLS LING CHANNEL TO PURUY PUND

INAME ISTACE TACTO 1518 STURN ISPHAI 158 e se 1746 TOPE 0.0 C RUCIING UNIA LAG AMSKK SECUN STAPE I COMP AV6 0.0 0.1 1.055 J.J

NORMAL DEPTH CHANTEL ROUTH IS

REMIM 5EE 2000 24f1) 28f2) 34f5) EL2VI ELMAK 0.3600 0.0400 0.000 143740 1443.0

CR35S SELTION COURJINATES--STAFFLEW, MA, LLEW--EIL 0.0 1440.00 190.00 1820.00 270.00 170.00 1418.00 280.00 1415.00 285.00 1415.00 295.00 1418.00 300.00 1420.00 450.00 1440.00

ST BRADE	41.27	03.12	H2.24	102.99	123.42	150.19	111.48	01-102	44.057	111.12
0.0161.34	0.1 6495.51	3.7 - (1)	0.0 14158.45	0°0 0°0 143*651	5.05	\$6.09 \$1080.03	357.44	1003.80	2349.51 50310.40	4 35 3 - 0 4 00 4 4 5 0 0 0
STAJĒ	1409.30	1510.55	1412.26 1426.26	1413.49	1415.53	1417.16	01.ct+1	1425.42	1422-35	1423.68
FLOM	0.ŭ 6435.Su	. č.č 13154.16	0.0 14158.45	0.0 18346.95	5.05	\$0.98 \$1080.03	357.44 34320.20	1050.88	2369.51 503/0.05	4321.64 00481.00
MAKTHUM STAGE TS"		k								
	•		*******	•	6	• • • • • • • • • • • • • • • • • • • •		• • • • • • • • • • • • • • • • • • • •		
4	; ; ;		NS	BTAREA RUNDE	SUBTAREA ROMOFF COMPUTATION	:				
		KA WEE HY	MUSERPH TO PURDY PUND	URDY YURD				:	1	
		-	STAU ICUMP B 0	1ECUN J	HAPE JPLI	JPRI	INAME ISTAUL	1041		
	99 4H1	26 4JHG	1AKEA S	HYURUGKAPH JATA SNAP TRSUA TRSPC 6.0 1.85 0.0		HATTU ISNUM	13AME LUC	FUCAL		
	LROFT	STRKR DLTKR	0.) 1.00	LUSS UATA PRATH STRKS 0.0	UATA KS TRTIOK U L-UU	STRIL	ALSHK 0-0	RT I HP		
	CURVE 15	(e	-71.00 WETNESS	'n	=1.00 EFFECT CA =-	71.00				
		!	- 10:	UNII HYDRUGHAPH DATA	GE I.35					
			STRTUE -	RECESSI -1.50 GRCSn	RECESSION DATA QRCSN= -0.35	KT1UR = 2.00				
0 M-3. 0.A	N. W.	PERIUJ TAIN	EXCS LUSS		POTON DE DE JERON TOUN	LUM HU.UA HR.THN PERIUU	HALF	exes Tuss	ב שאטי	
						:	503 6-43 5	3.22 3.18 82.11 81.11	23605. (a75.78)	SHEET
	***		***		****	*****	,		! ! ! !	18
				CUMBINE HYJRUGHAPHS	URUGHAPHS					OF
	!	11911年出	CLIBILE HYDROGRAPHS FROM STATIONS 7 ALO 6	TOH STATIONS	7 A.10 6					2

HYDRUGRAPH ROUTING

ייי											
		15.740	ICUMP 1		ITAPE O	JALT	D S	INAME	JPRT INAME ISTACE TAUTU	Uaulu 0	
	41.053	0.0	A V G		IRES ISAME	10p1	0 M d I		LSIR		
		ASTPS NSTUL	NSTUL		AMSKK 0.0	×	15K STURA 15PRAT	S TURA -	I SPRAI		
STAGE 1:09.00 Le	1.99.70	161	1410.50	14.1.30	1		1412.10	:	i		
FLUX 0.0	_01:22		67.40	114.70	176.73	01.	246.70				
SURFACE AREA= 11.	12.		39.	.69							
CAPACITY: 0.	54.		318.	1378.				:			:
EL EVATION# 1404;	1.000	.0241		1440				!			
	UREL 1 + J 9 2 . J	SPM10 7 0:0 -		CU3M EXF	EXPW ELEVL		LUUL LAKEA 0.0 - 0.0 -		LXPL J.D.		
	Ì				3	AIA					
				1409-6 3-1		LAPO DAMMID	0.4Mm.I.U-				
CREST LENGTH OT TO				57:			58.	73.	18:		
ELEVATION 1409.0		1413.0	1410.5	1411.0	1411.5		0-7141	1412.5	1413.0		
PEAK GUIFLING IS 1774. AT TE	1	4E 7.50 HOURS	40 URS								
		•							:		
		********					**********			*****	

OPERATION S	STATION	AKEA	PLAN RATTO	1 01	RAT	RATIUS APPLIEU TU FLUMS	EU TU FLU	24					
нузясмарн ат		2.461	1	30.4416									
RDJFEJ TO	, ²	7.93 - <u>6</u> 65.7	1 -1	17.871	1 1		! ! !		:				
R0JFEJ TO	-	2.461	-	15.7111									
HYDEOGRAPH AT	*	126.6		74.6911	!		1						
2 (04814E)	2	12.381	1 1	3057.									
ROUTED TO	9	15.381	1	832. 23.5516					1				i
ROUTED TO	1	12:381	7	23.5211									
HYDROGRAPH AT	e -	(8.1	1 4	1540.					:			:	
2 COMBINED	٥	17.11	1	1886.									
ROUTEU TO	0.1	 17.11)5 <u>L</u>	56.2311			:		!		!		
•			:	† † † † † † † † † † † † † † † † † † †			:	1	:				SHEE.
							: .	!		† :			:0
													OF
	1	!				1		-		-			!

SUMMARY OF DAM SAFETY ANALYSES

PLAY	1 (11166) Lang. Var.	ELEVATION STORAGE	1N111AL VALUE 1537.00 61.		SPILLMAY LMEST 1537.00 61.	•	10P of UAA 1554-60 Elfe: 571.	: : :	:	
	RATIO OF Dur	AAXI 1UH AESEAVOIR	MAXIMUM OEPIH JOER DEN	HAX I MUH SI UKAGE	MAX1AUM COTFLOR	DURATION OVER TOP RIURS	FIME OF MAX UNIFEUM	TIME OF FALLORE HEURS		i :
•	70.1	1540.16	0.56	128.	031.	1.01	7.00	2.2		
			ā	PLAN 1	SIATIUN	ا ا			:	
		1	RATIO	MAKINUM FLUM,CFS	MAKINUM STAGE: FT	11ME HOUKS				İ
			1.00	555.	1484.3	1.33				
İ										ļ
:										
				i : :	:		i i			:
!										} !
			5			1	!			i
			1		!	•				
			1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1						MEET
					,	1				- 21
										o F
;				!						z

SUMMARY OF DAM SAFETY ANALYSIS

HE OF ALUNE HOURS
1 T E
HOURS
79.7
2 200
·

SUMMARY OF DAM SAFETY ANALYSIS

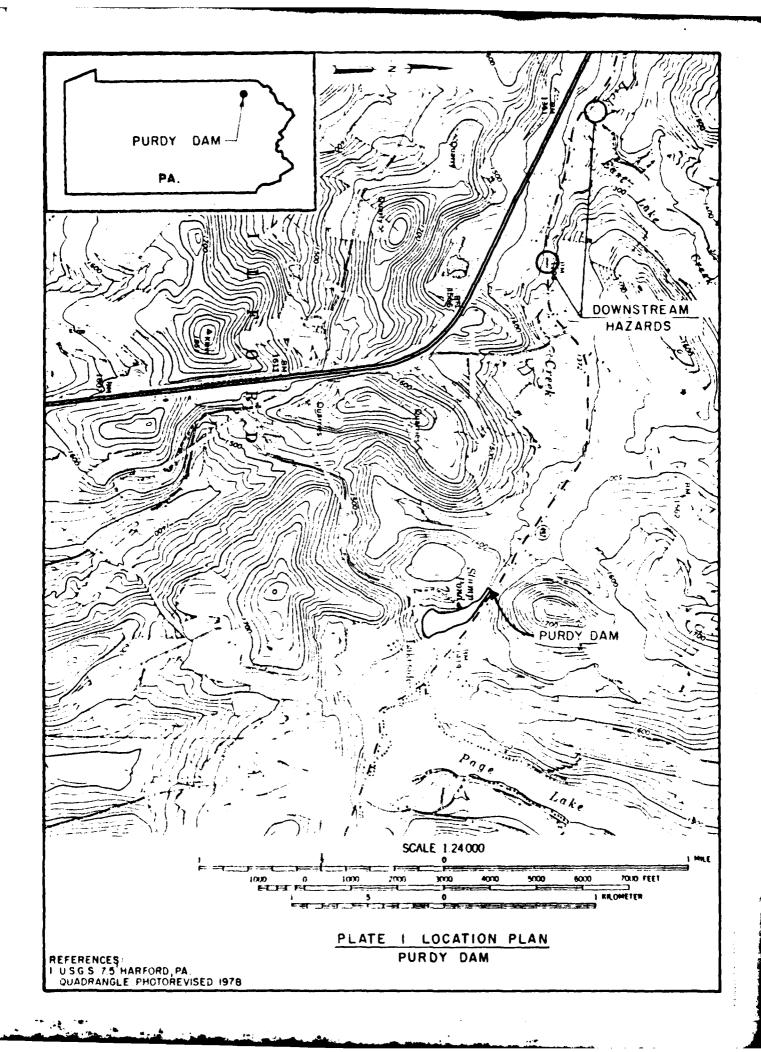
	RAIIU OF 100	UNIFUM MAXIMUM OF ALSENDIR DEPTH OF ALSENDIR DEPTH OF ALSENDIR DATH OO 1413.92 4.32	HAKIMUM HAKIM DEPTH STUKA UVER DAM AC=F 4.32 13	9 9 9 9	MAXIMUM DU COST COST COST COST COST COST COST COST	DURATION THUKS 40.83	ATHE OF MAX OUFFLUE HUURS	ITHE OF FALUKE HOURS	
	1.00 / / / / / / / / / / / / / / / / / /	4AX1 4UM 4.5EX 4018 4.5.5EEV 1413.92 1413.92	MAXIMUM DEPTH JVER DAM 4.32 4.32 MOUTING	NAXIMUM STOKAGE AC=F7 L36.	HAKIAUH GUIFLUE CFS 1774*	DURATION THURS 40.43	AAX GUTTUN HUURS 7-30	FALUKE FALUKE HUUKS U.O	
	1.00	1413.92	4.32 Bouring	961	11114.	20° 0.	1,50	0.0	
	1.00-7	GAR. From	Bouring						
	1-00/	GAR Troop	Rourins						
1									
	•	1			! : !				
				į					
i i									;
1	i i i		1						
•						• · · · · · · · · · · · · · · · · · · ·			:
		:				!	1		

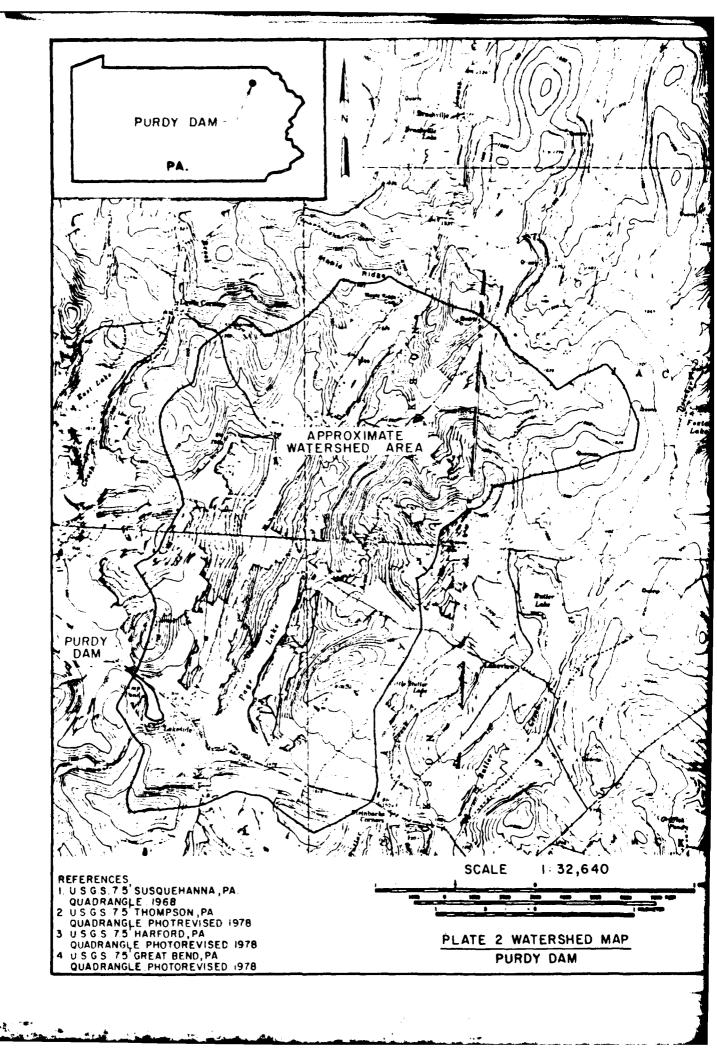
APPENDIX E

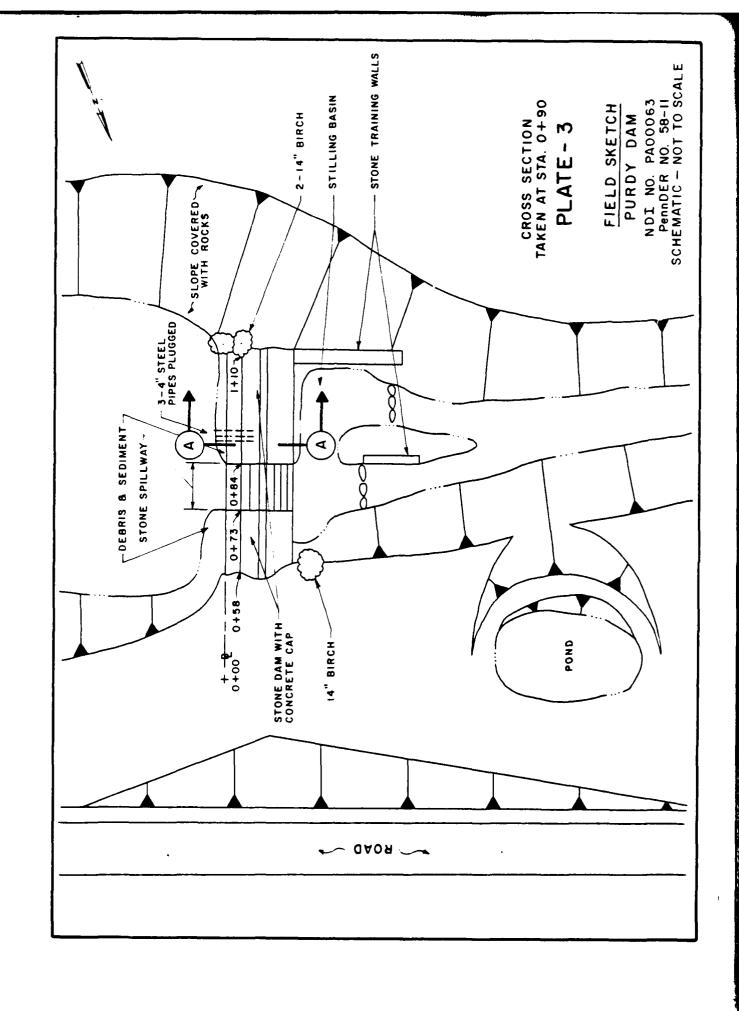
PLATES

CONTENTS

- Plate 1 Location Plan
- Plate 2 Watershed Map
- Plate 3 Field Sketch Plan from Field Inspection
- Plate 4 Top of Dam Profile and Typical Cross Section from Field Inspection







APPENDIX F

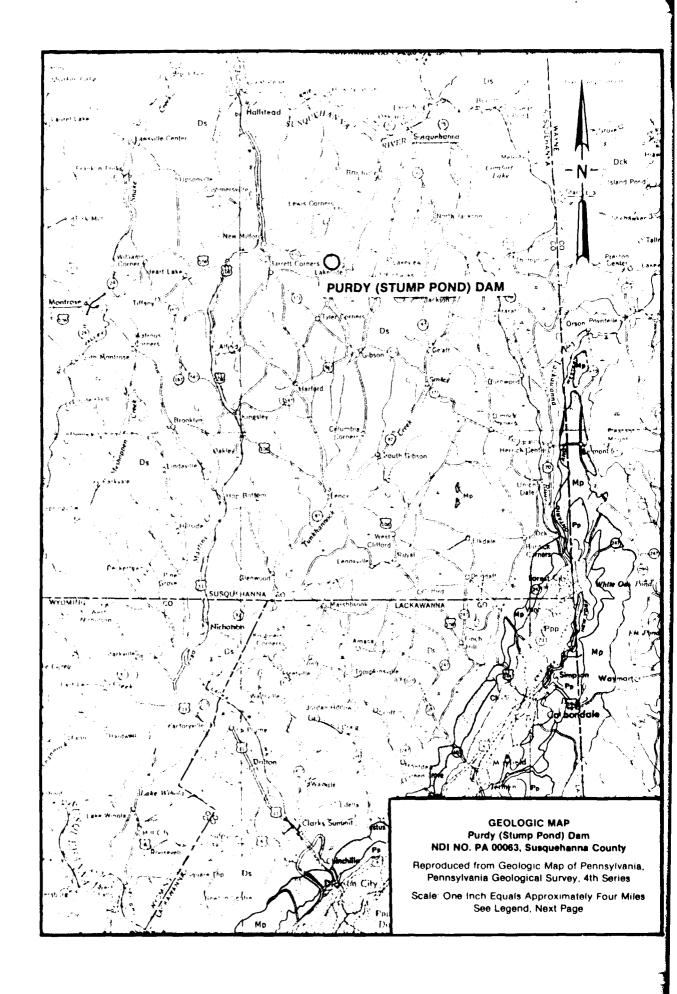
REGIONAL GEOLOGY

PURDY (STUMP POND) DAM NDI No. PA 00063, PennDER No. 58-11

REGIONAL GEOLOGY

Purdy Dam is situated in the Glaciated Low Plateaus physiographic province. The area has undergone glaciation at least three times and is presently covered with Wisconsin stage glacial deposits. According to the Soil Conservation Service's Soil Survey for Susquehanna County, the surface soils consist primarily of slightly stoney, silt loams of the Morris-Wellsboro-Volusia association. No test boring data were available for review, thus, the thickness of this overburned is difficult to ascertain.

Geologic references indicate that the bedrock in the vicinity of the dam consists primarily of members of the Catskill Formation in the Susquehanna Group. These are chiefly red and gray shales and sandstones of Upper Devonian age. The formation also contains scattered, thin, coal streaks and scattered fish remains. A bedrock sample obtained at the dam site was a hard olive green, fine grained sandstone. The strata in the area were deposited in a bay or delta front environment and remained essentially horizontal after the Appalachian Uplift.



GEOLOGY MAP LEGEND

DEVONIAN UPPER

WESTERN PENNSYLVANIA

Don Or

Det

Oct

(X)

Oswayo Formation

the ends gray logray shares, substants and
son thinks beloning coverage of a shall
us shared considered equation of a few coverage. Received Formation of a few and Commod countries probably not
distinguishable north of Corry

Cattaraugus Formation

CALLALAURUS FORMATION
Red, gray und bryan while and mindstone with the proportion of red decreases in resident decreases a west acted accordence becomes superior rate of Saturmation strates in a real resignation of the some timest one real confidence counterface of the some timest one real conditional for counters.

Conneaut Group

Connectic Comp.

Microstrop wing, brown, greenish and superich whiles and substances includes pink rows of triffere and "Cheming and "Green's Founttions of methics for Pennsylvania".

Canadaway Formation

Afternating broan shales and sandstones in ados "Portuge". Femation of north western Procsyvania

Dho

CENTRAL AND EASTERN PENNSYLVANIA

Doo

Oswayo Formation

OSWBYO POFIBBLION
Brownsh and greensh gray, fine and
induce ground samistions with some shirts and soutlevel solarous leave, white and shales which home more nameous customed. Relation to type covering and protect.

Dck

Catskill Formation

CAISKIII FOIMBLION Cheefly red to brownish shales and sand-stones consider gray and greenish son to stone longues named Eth Mountain, Honestale, Shahola, and Delaware River in the cast.

Marine beds

prairie 1993.
Gray to dive brown shales, grayworkes, and sands one contition. Cheming both and Plattage bads including limited, Brather Haveth, and Telimiers Ross. Puly Line stone at bose.

0.5

Susquehanna Group

Raibed line is Chaming Cutskid can-test of Second Processitives Survey County reports barbs on Cheminy side of line

MIDDLE AND LOWER



Mahantango Formation

MERICANCY FORMATION
RESSON to obve shife with interbedded
smithtones which are dominant in places
(Montebella) highly fossificious in upper
part contains "Conferfield coral bed" in
easter Pennsylvania

Marcellus Formation

otherwise a continue of the with thick, brown sandalone (Purkey Redger en parts of central Pennsylvania)

Onondaga Formation

Onondaga Formation
Greenish Bise, thin bridged shale and dark
blue to black medium bedded limitions
with shale predominant in most places,
includes Selinsgione Limestone and Need
more Shale in central Peningliania and
Butternik Falls Limestone and Esopia
Shale in easternmost Piningliania, in
Lehish Guy area includes Palmerton
Sandstone and Howmanstonen Chert



Do

Dhb

Oriskany Formation

CPINKBIY FOFTIBLION
White to beaun, then to course grained, partly characteristic healthy could metally, tossistic to saintiffering the grain through the saintiffering the grain shortly length or with some constituted shalls and saintiffing beautiful the saintiffering beautiful through the saintiffering beautiful through the saintiffering beautiful through the saintiffering beautiful through the saintiffering beautiful through the saintiffering beautiful through the saintiffering t



Dh

Hamilton Group

Helderberg Formation

Helderberg Formation
Thack group, and accounts them bedded shale
"Manufathed at the top, equivalent to Port
keep Shale and He earl Female in 'in the
last dark group cheefe. Thin bodded,
toostile town Timestone. (New Neutrand)
with some hand sometismes in the middle
gold, at the loss office arms, medium to
thick bodded explicitline. Innection
to against semigranishaly in places with
some heef modules.

